

Workshop Cargèse

Trends in physical and numerical modeling of multiphase flows,
CFD and its experimental validation for multiphase flows
IESC Cargèse 2012, sep 24-28 2012

Lagrange-remap solver and low-diffusive interface capturing for air-water flows

Aude Bernard-Champmartin^{1,2}, Florian De Vuyst¹

1: CMLA, ENS Cachan / LRC MESO

2: CEREMADE, Université Paris Dauphine

Outline

1. System of interest
2. Numerical method
3. Antidiffusive procedure for the interface
4. Numerical experiments & validation
5. Concluding remarks

System of interest

- Air-water multifluid flow
- Viscous effects neglected
- Surface tension neglected

- Transport equation to track the mass gas fraction transport c_g

- « Three-equation » volume averaged model (one velocity) with pressure equilibrium closure

Scope, applications, project

- Wave breaking/wave impact analysis
- Pressure impact under sloshing conditions
- Pipe flows

- ... a milestone before including more Physics (viscosity, surface tension, ...)
- ... prototype multiphase code solver suitable for GPU parallel computing.

System of equations

- Isentropic Euler system for gas
- Isentropic Euler system for (compressible) liquid
- + interface (kinematic/dynamic) conditions

- Trick : make use of a colored fluid function

$$\partial_t z + \mathbf{u} \cdot \nabla z = 0, \quad z \in \{0, 1\}.$$

- Numerical approach: consider

$$\partial_t z + \mathbf{u} \cdot \nabla z = 0, \quad z \in [0, 1]$$

- Use the mass gas fraction for example as color function:

$$\partial_t c_g + \mathbf{u} \cdot \nabla c_g = 0, \quad c_g = \frac{\alpha \rho_g}{\rho}$$

$$\alpha = \text{gas void fraction}, \quad \rho = \alpha \rho_g + (1 - \alpha) \rho_\ell.$$

- We get mass conservation per phase :

$$\partial_t(\alpha \rho_g) + \nabla \cdot (\alpha \rho_g \mathbf{u}) = 0,$$

$$\partial_t((1 - \alpha) \rho_\ell) + \nabla \cdot ((1 - \alpha) \rho_\ell \mathbf{u}) = 0,$$

- + momentum equation

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla p = \rho \mathbf{g}$$

- + closure : pressure equilibrium closure:

$$p = p_g(\rho_g) = p_\ell(\rho_\ell) \longrightarrow \varphi(\alpha) = 0.$$

Choice of the EOS for each fluid

- For the gas phase, we use a *perfect gas law* :

$$p_g(\rho_g) = p^0 \left(\frac{\rho_g}{\rho_g^0} \right)^{\gamma_g}, \quad \gamma_g = 1.4, \quad \rho_g^0 = 1.28 \text{ kg/m}^3, \quad p^0 = 10^5 \text{ Pa}.$$

- For the water : we use a *modified Tait equation* for the liquid

$$p_\ell(\rho_\ell) = p^0 \left\{ 1 + K \left[\left(\frac{\rho_\ell}{\rho_\ell^0} \right)^{\gamma_\ell} - 1 \right] \right\}, \quad K = \frac{\rho_\ell^0 c_s^2}{p^0 \gamma_\ell}$$

with for instance: $\gamma_\ell = 3.5$, $\rho_\ell^0 = 1000$, $c_s = 350 \text{ m.s}^{-1}$, ($K = 350$)

NB: weakly compressible: if $p = \frac{p^0}{2}$, then $\rho_\ell = 999.59$

Pressure equilibrium equation

- From the knowledge of the conservative variables $W_g = \alpha \rho_g$ and $W_\ell = (1 - \alpha) \rho_\ell$, we have to solve :

$$p_g(\rho_g) = p_\ell(\rho_\ell)$$

i.e.

$$\varphi(\alpha) = \left(\frac{W_g}{\alpha \rho_g^0} \right)^{\gamma_g} - 1 - K \left[\left(\frac{W_\ell}{(1 - \alpha) \rho_\ell^0} \right)^{\gamma_\ell} - 1 \right] = 0, \quad \alpha \in]0, 1[.$$

- NB : very stiff function, the choice of the iterative solver requires attention (initial guess, surrogates, Newton, etc.)
- In fact, there is a trick ... :

Trick for initial guess :

- The liquid mass conservation equation can be written in the form :

$$\partial_t(1 - \alpha) + \nabla \cdot [(1 - \alpha)\mathbf{u}] = -\frac{D_t \rho_\ell}{\rho_\ell}.$$

- Under the *weak compressibility assumption* or the liquid phase, we get

$$\partial_t \alpha + \nabla \cdot (\alpha \mathbf{u}) = 0.$$

- A numerical scheme is applied to this additional "guess equation" to compute initial guesses of the iterative solver
→ Newton algorithm converges in 2 iterates with acceptable accuracy (**strong improvement in CPU time**).

Numerical scheme

Lagrange-remap strategy

- First write the equations in **Lagrangian** form

$$\frac{d}{dt} \int_{\Omega_t} \alpha \rho_g dx = 0,$$

$$\frac{d}{dt} \int_{\Omega_t} (1 - \alpha) \rho_\ell dx = 0,$$

$$\frac{d}{dt} \int_{\Omega_t} \rho \mathbf{u} dx + \int_{\Omega_t} \nabla p dx = \int_{\Omega_t} \rho \mathbf{g}.$$

(Lagrange integral form here)

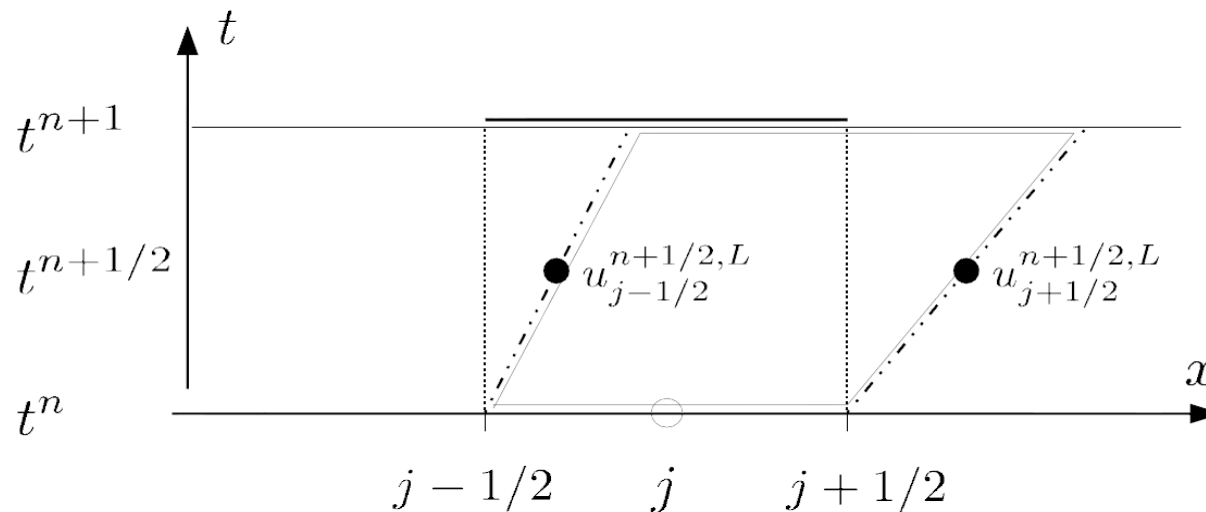
- Integrate them in time over a time step
- **Project** the quantities on the fixed Eulerian grid (remap)

Conservative form

- Lagrange-remap schemes can be rewritten actually in conservative form [De Vuyst et al, CRAS Mécanique 2012].
- 1D case :

$$(\alpha\rho_g)_j^{n+1} = (\alpha\rho_g)_j^{n+1} - \frac{\Delta t}{h} \left[(\Phi_{m,g})_{j+1/2}^{n,n+1} - (\Phi_{m,g})_{j-1/2}^{n,n+1} \right],$$

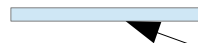
$$(\Phi_{m,g})_{j+1/2}^{n,n+1} = \alpha_{j+1/2}^{n+1,L} (\rho_g)_{j+1/2}^{n+1,L} u_{j+1/2}^{n+1/2,L}$$



Antidiffusive strategy

$$(\alpha\rho_g)_j^{n+1} = (\alpha\rho_g)_j^{n+1} - \frac{\Delta t}{h} \left[(\Phi_{m,g})_{j+1/2}^{n,n+1} - (\Phi_{m,g})_{j-1/2}^{n,n+1} \right],$$

$$(\Phi_{m,g})_{j+1/2}^{n,n+1} = \alpha_{j+1/2}^{n+1,L} (\rho_g)_{j+1/2}^{n+1,L} u_{j+1/2}^{n+1/2,L}$$



Void fraction at interface :
how to compute it ?

- Strategy : « be as sharpest as possible for step-shaped color functions while staying stable (just at the limit) »
- Idea : design a combination of upwinding scheme and **downwind** scheme [Lagoutière Després 2002, Kokh-Lagoutière 2010]
- The advection process can be seen as a over-compressive « limiting » procedure (superbee-like, hyperbee, ...)

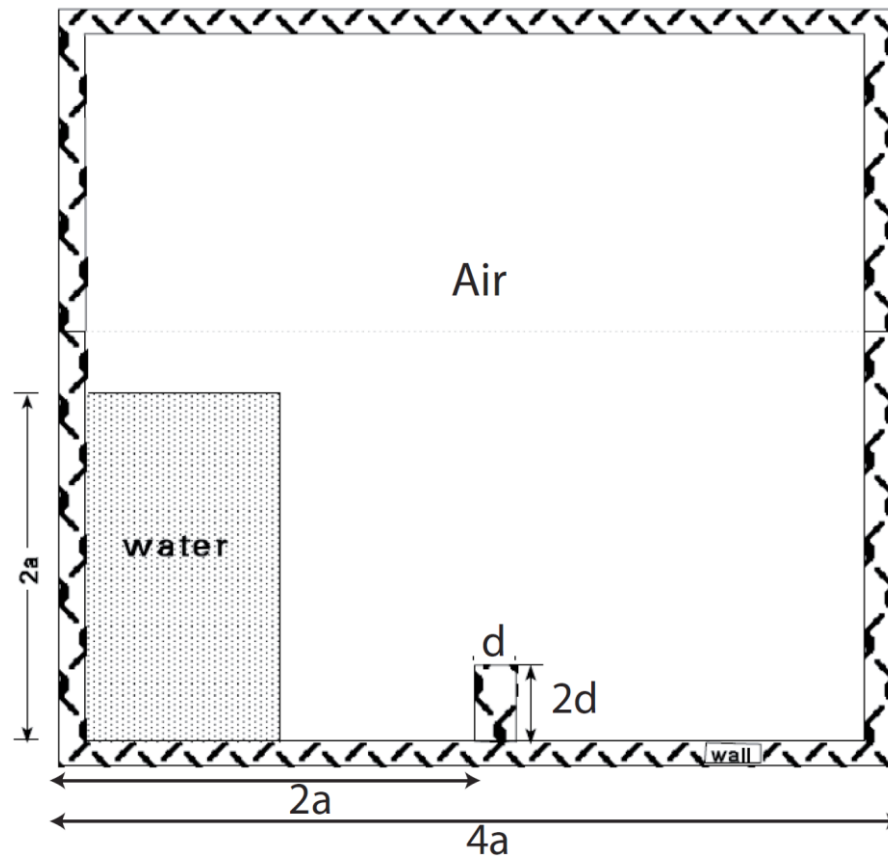
Test cases

and numerical experiments

(+ comparison to physical experiments
for some of them)

1. Collapse of a liquid column with an obstacle

O. Ubbink Numerical prediction of two-fluid systems with sharp interfaces, PhD thesis (1997)



$$a = 0.146 \text{ m}, d = 0.024 \text{ m}$$

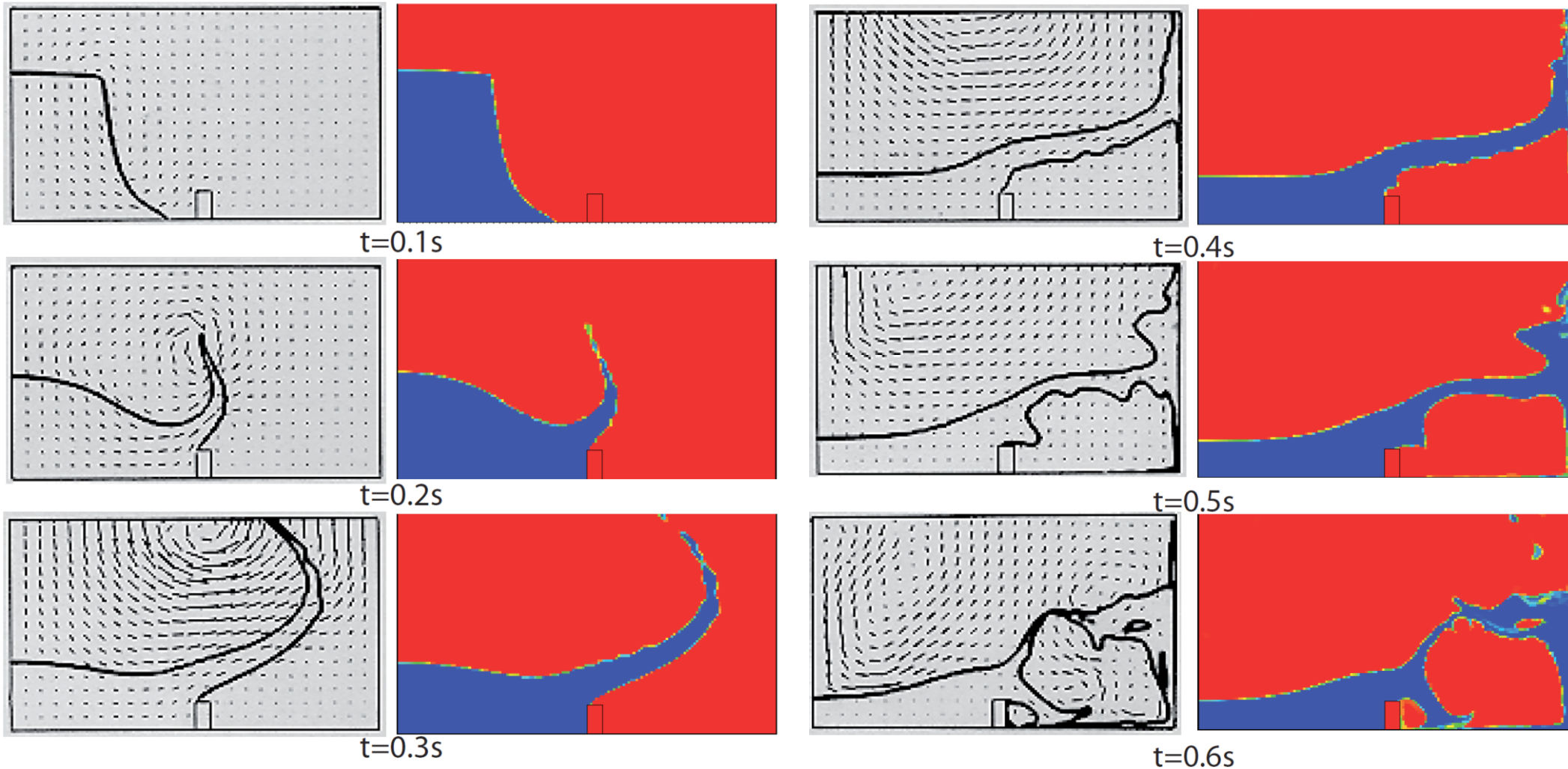
$$N_x = N_y = 150$$

$$\gamma_g = 1.4, \gamma_l = 7$$

$$\rho_0^g = 1.28 \text{ kg.m}^{-3}, \rho_0^l = 1000 \text{ kg.m}^{-3}$$

$$P_0 = 10^5, c_{\text{sound}} = 350 \text{ m.s}^{-1}$$

Collapse with an obstacle – comparison with incompressible fluid model



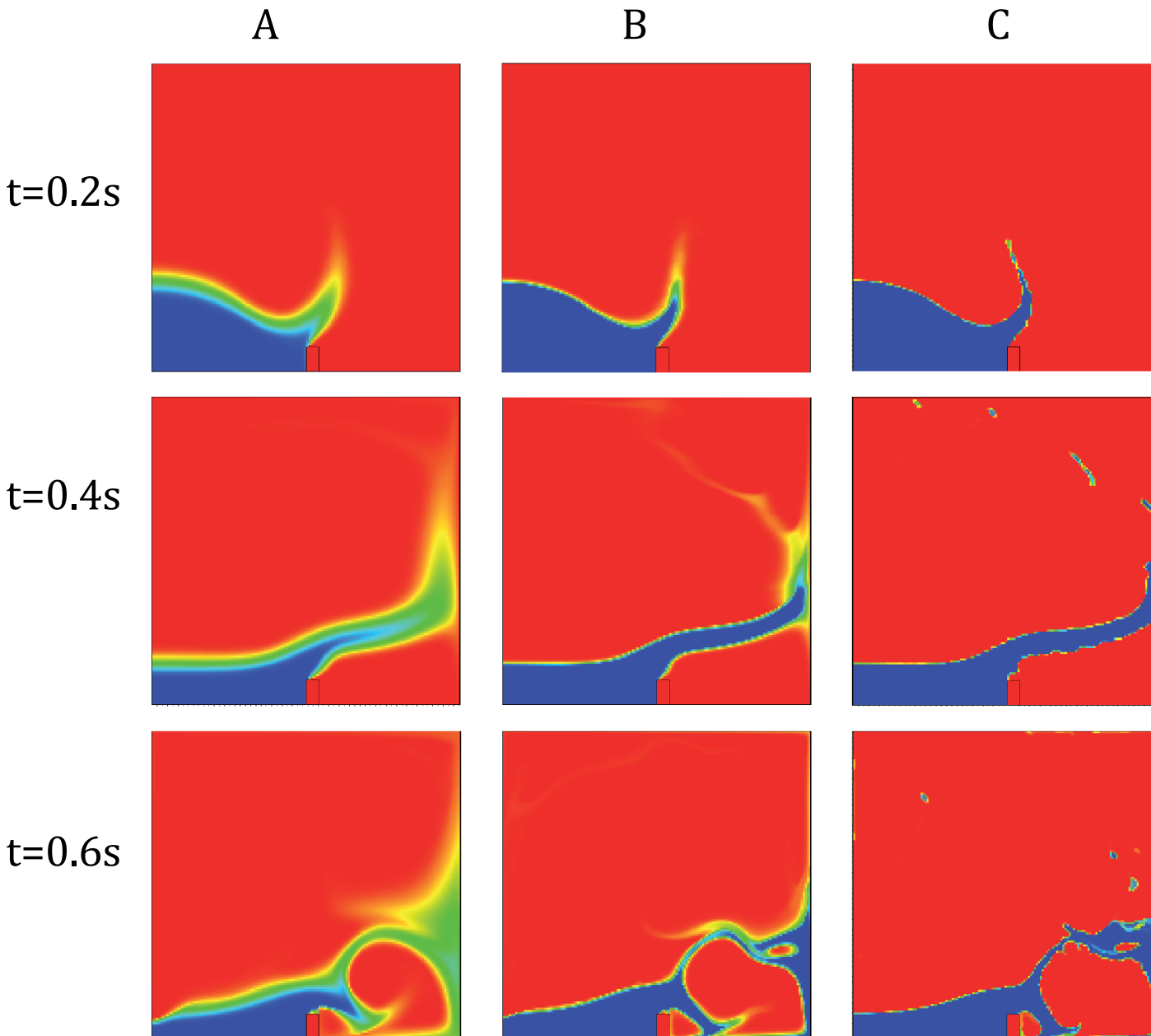
Num. Result.
Ubbink

Num. Result. with
Odyssey

Num. Result.
Ubbink

Num. Result. with
Odyssey

Benefits of the antidiffusive approach

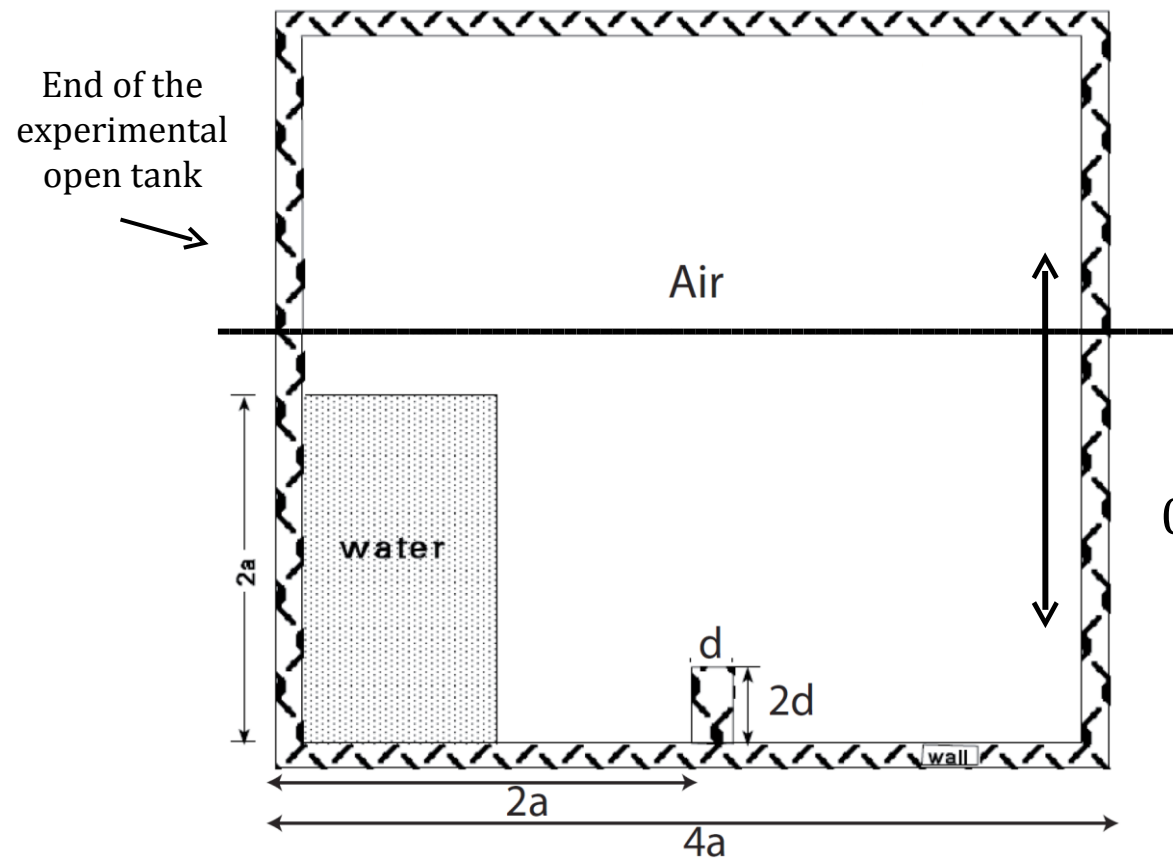


Evolution of \checkmark for
different remapping
algorithms

- ✓ Case A: 1st order with upwind
- ✓ Case B: 2nd order with upwind
- ✓ Case C: 1st order with Low-Diff.

- Another case of collapse of a liquid column with an obstacle

D. M. Greeves Simulation of viscous water column collapse using adapting hierarchical grids J. Num. Meth. Fluids 2006



$$a = 0.25, d = 0.04$$

$$L_x = L_y = 1 \text{ m}$$

$$N_x = N_y = 300$$

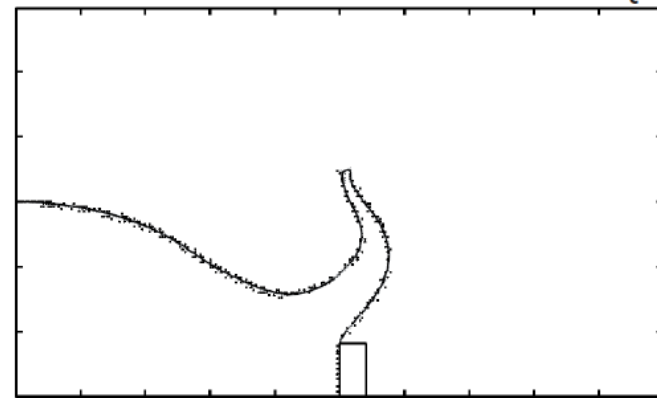
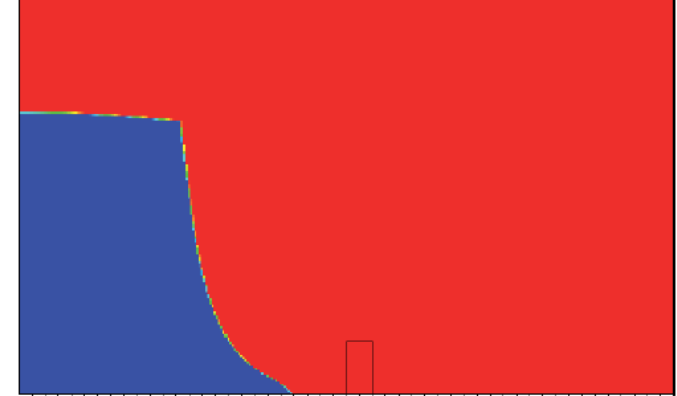
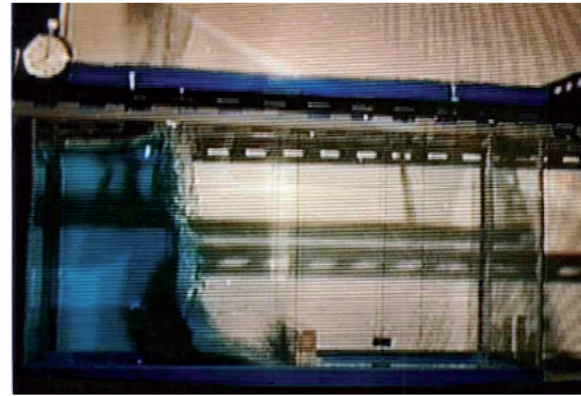
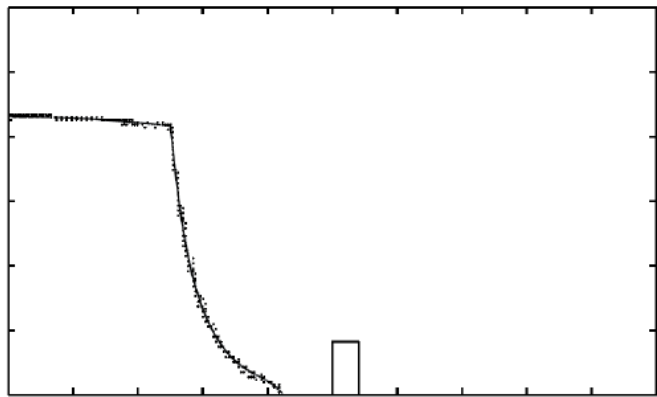
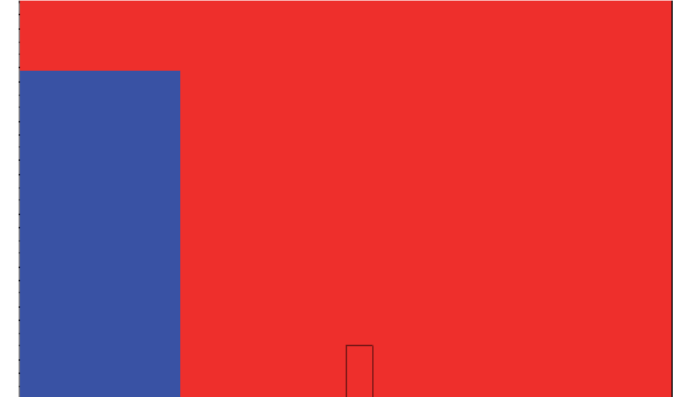
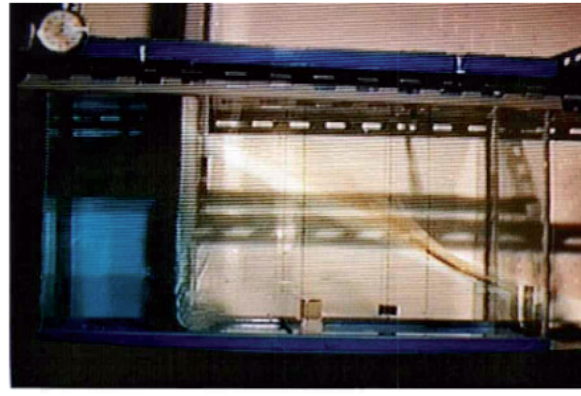
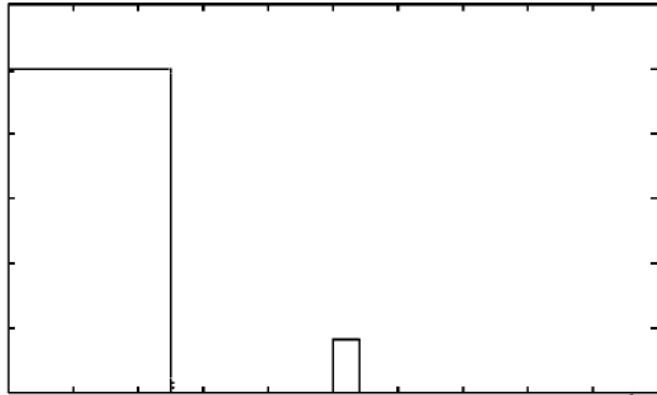
$$\gamma_g = 1.4, \gamma_l = 7$$

$$\rho_0^g = 1. \text{ kg.m}^{-3}, \rho_0^l = 1000 \text{ kg.m}^{-3}$$

$$P_0 = 10^5, c_{\text{sound}} = 350 \text{ m.s}^{-1}$$

Exp: from
Koshizuka et al A particle method.. Comp. Fluid Mech. 1995

Simulations of a dam break



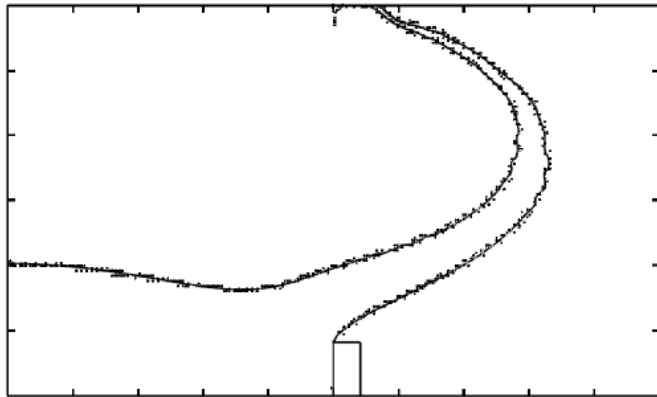
Sim. Greeves

$t=0.258s$

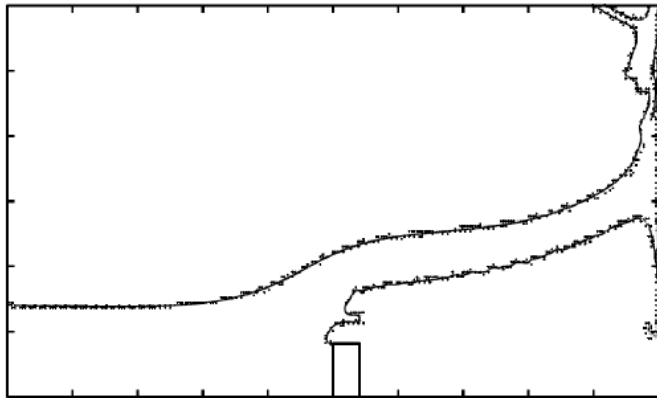
Exp. Koshizuka

Sim. Odyssey

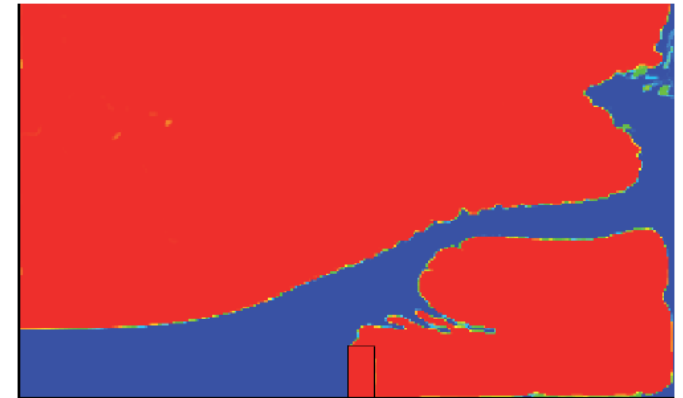
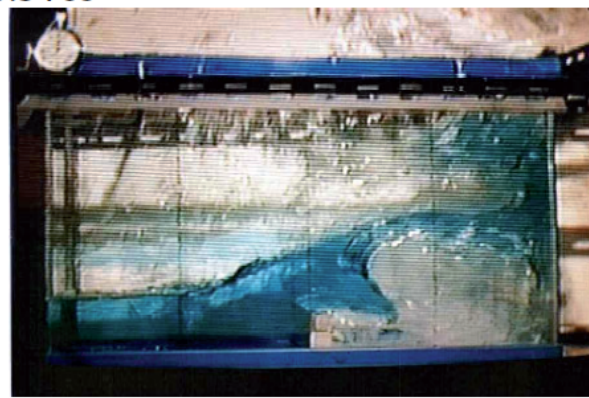
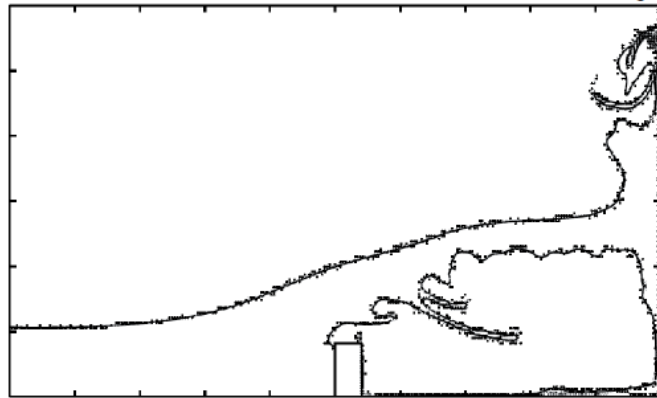
Simulations of a dam break



t=0.387s



t=0.516s



t=0.645s

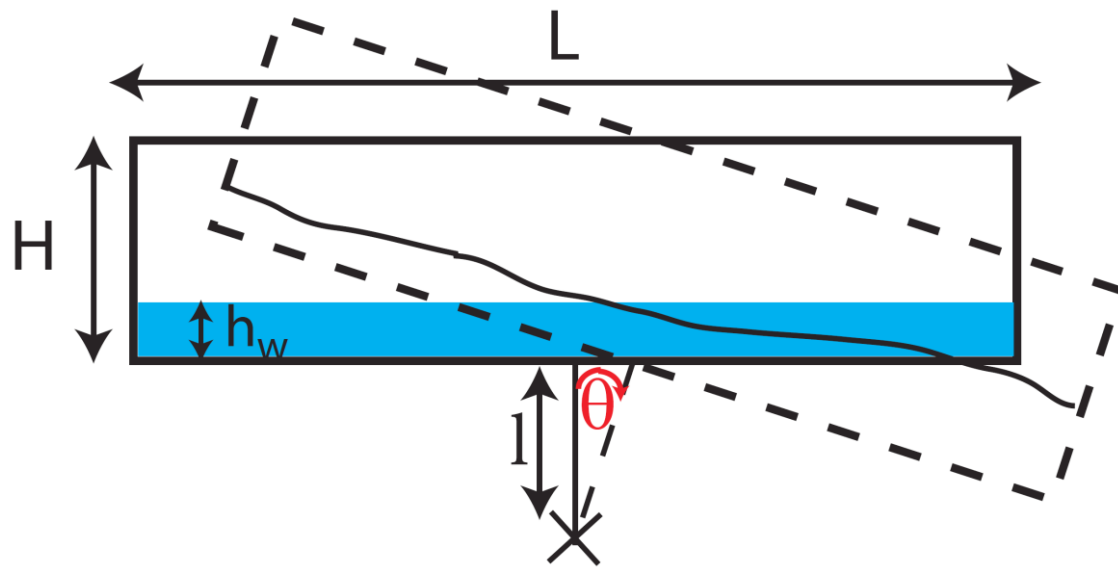
Sim. Greeves

Exp. Koshizuka

Sim. Odyssey

Sloshing test cases – pitch motion

- Sloshing due to the **pitch motion** of a rectangular tank:



J.R. Shao *et al.* An improved SPH method for modeling liquid sloshing dynamics. *Comp. Fluids* 2012

$$L = 0.64m, H = 0.14m, h_w = 0.03m$$

$$N_x = 300, N_y = 67$$

The tank is oscillating as a **pendulum** according to:

$$\theta(t) = \theta_0 \sin(\omega_r t)$$

with $\theta_0 = 6^\circ$, $\omega_r = 4.34 \text{ rad/s}$ ($T = 1.45 \text{ s}$)

Simulation are performed in the frame of reference of the tank.

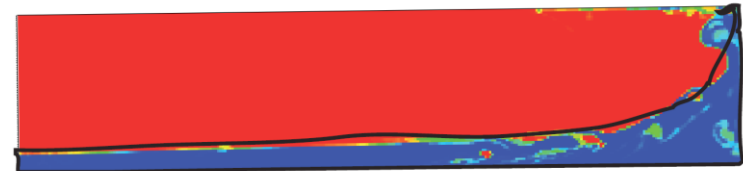
Comparison SPH – present method

We superimpose the profile of the article:

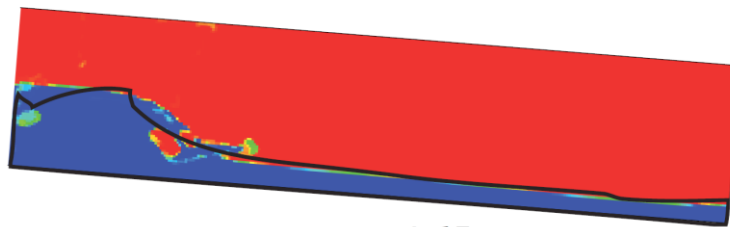
J.R. Shao *et al.* . An improved SPH method for modeling liquid sloshing dynamics. *Comp. Fluids* 2012



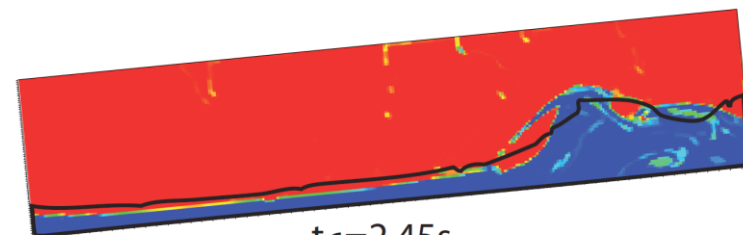
$t_1=1.45s$



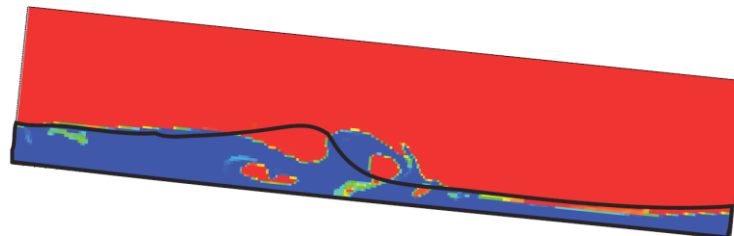
$t_5=2.2s$



$t_2=1.65s$



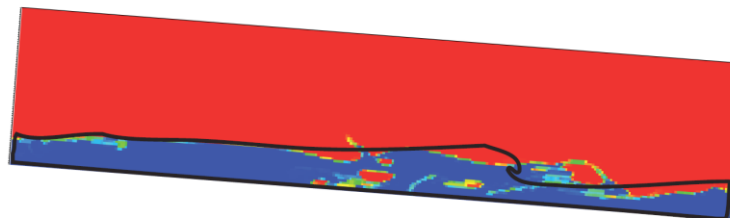
$t_6=2.45s$



$t_3=1.85s$



$t_7=2.65s$



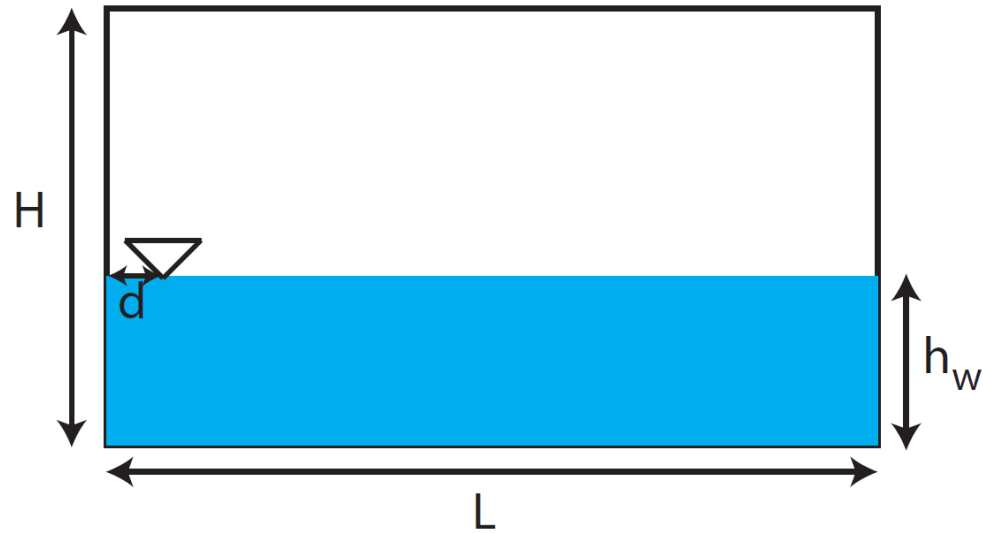
$t_4=1.98s$



$t_8=2.90s$

Sloshing test cases – surge motion

- Sloshing due to the **surge motion** of a rectangular tank:



J.R. Shao *et al.* An improved SPH method for modeling liquid sloshing dynamics. *Comp. Fluids* 2012

$$L = 1.73m, H = 1.15m, h_w = 0.6m$$

$$d = 0.05 \text{ m}$$

$$N_x = 173, N_y = 115$$

The tank is moving horizontally according to:

$$x(t) = A \cos\left(\frac{2\pi t}{T}\right)$$

with $A = 0.032 \text{ m}$, $T = 1.3 \text{ s}$ ($\omega_{forced} = 4.83 \text{ rad/s}$).

First natural frequency of the fluid
in the box

$$\omega_{fluid} = \sqrt{g \frac{\pi}{L} \tanh\left(\frac{\pi}{L} h_w\right)} \approx 3.77 \text{ rad/s}$$

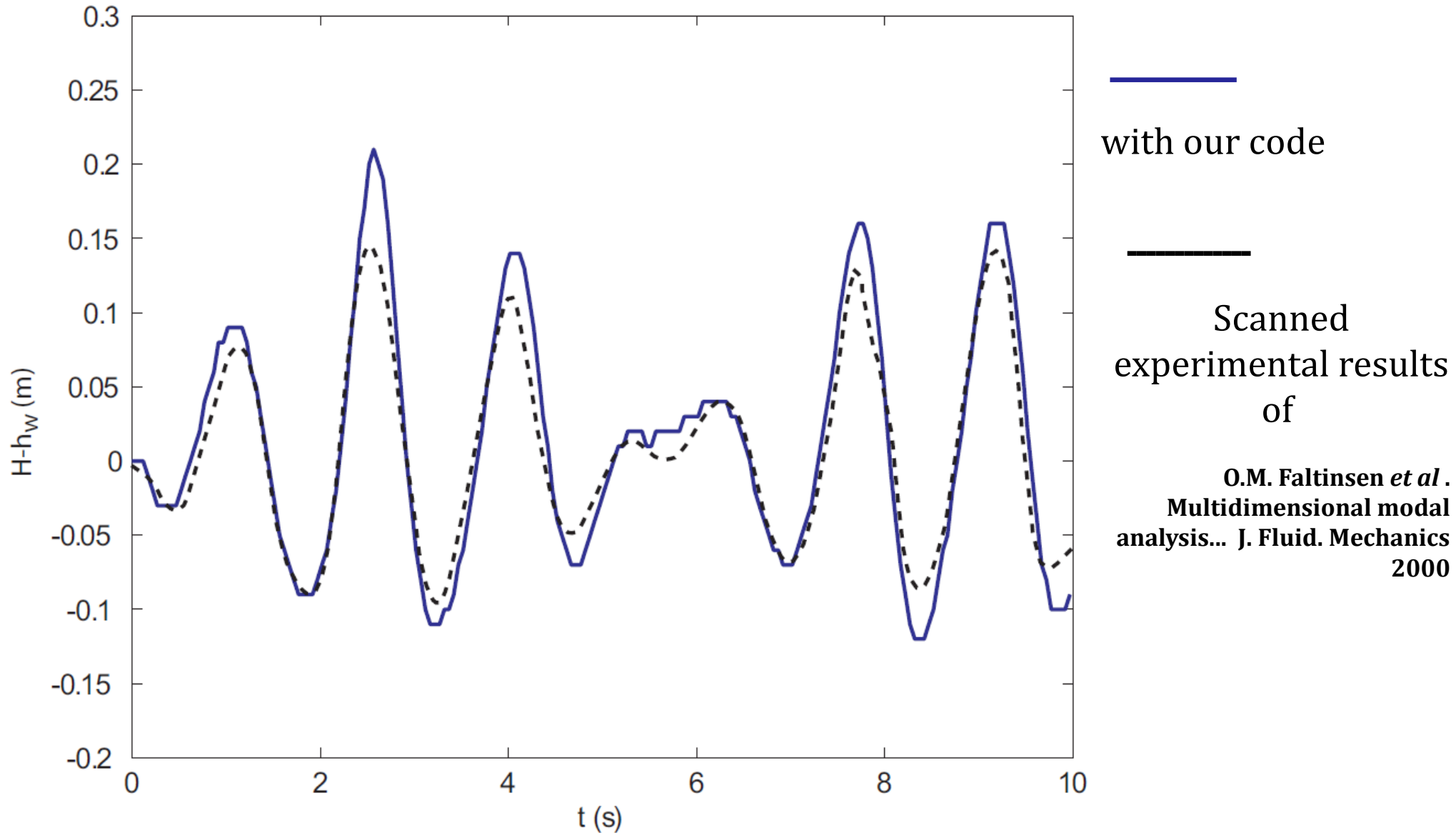
Two frequencies are acting ω_{fluid} and ω_{forced}

Experimentals results are available:

O.M. Faltinsen *et al.* Multidimensional modal analysis... *J. Fluid. Mechanics* 2000

Sloshing test cases – surge motion

Free surface elevation of water at the probe



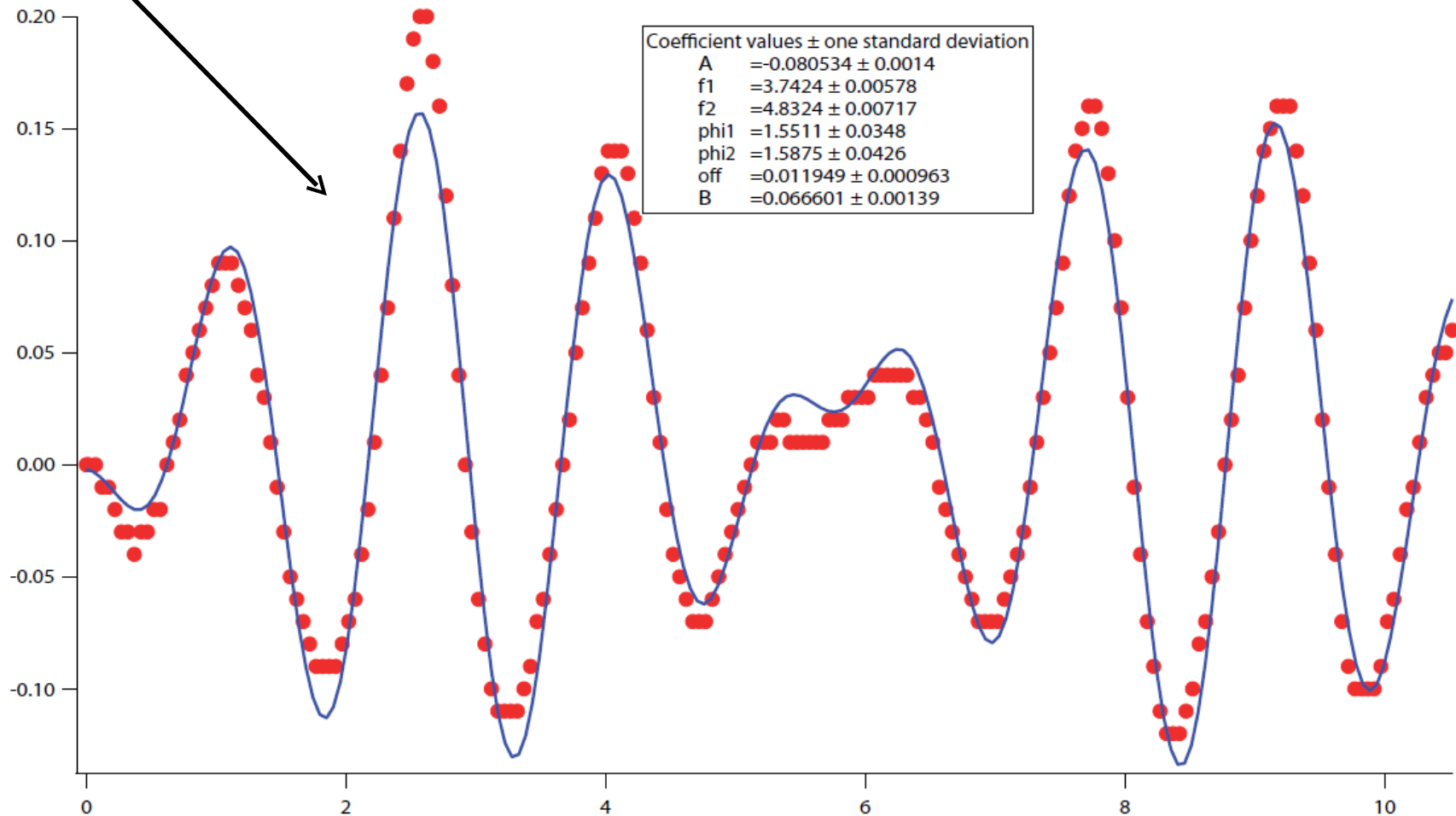
Sloshing test cases – surge motion

We search to **find a fit** of our curve with a function as a superposition of two signals

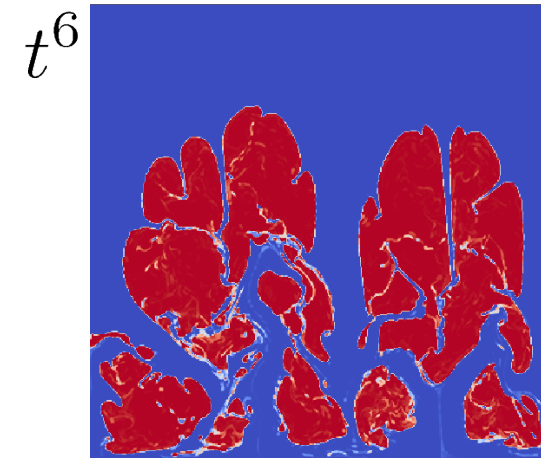
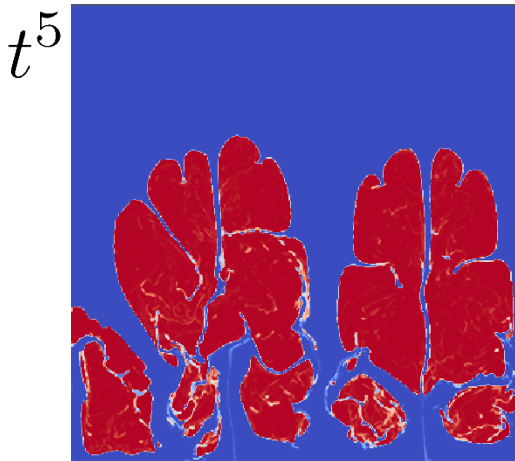
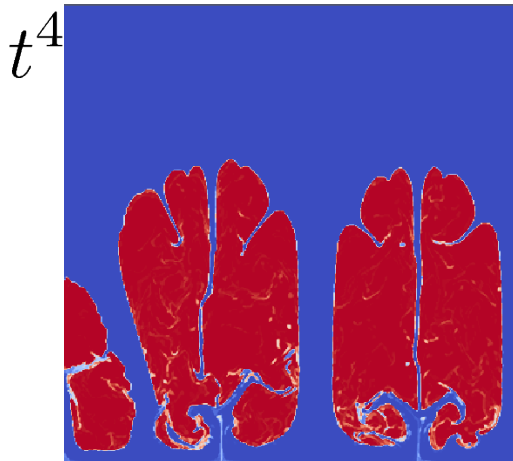
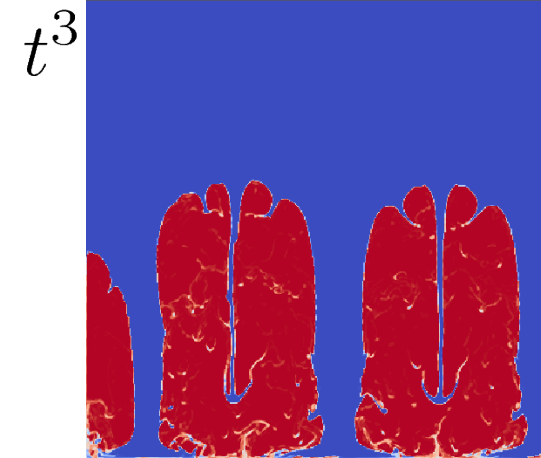
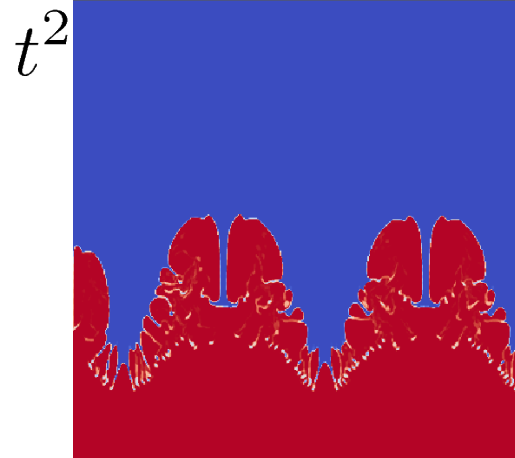
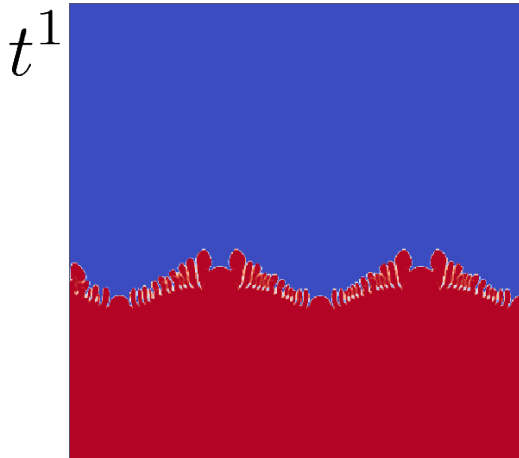
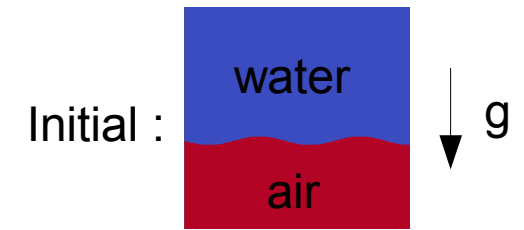
$$f(t) = A_1 \sin(f_1 t + \varphi_1) + A_2 \sin(f_2 t + \varphi_2)$$

we get: $f_1 = 3.74 \pm 0.01$ rad/s, $f_2 = 4.83 \pm 0.01$ rad/s

very close to $\omega_{\text{fluid}} \approx 3.77$ rad/s and $\omega_{\text{forced}} = 4.83$ rad/s



LT air-water Rayleigh-Taylor instability



About 0.5 sec of physical time

Grid 400x400, about 1.5 day of computation (sequential)

Concluding remarks

- Innovative numerical Eulerian method involving :
 - a Lagrange-Remap finite volume method
 - an anti-diffusive approach and the void fraction to keep a thin interface between the two fluids
- The test cases show a good agreement between XP and other codes (dam break, sloshing events)
- Ongoing works : XP + num of water wave wall impact (Luc Lenain, Ken Melville, U. Delaware San Diego, Frédéric Dias, U. College Dublin).
- Need to add : physical viscosity, surface tension for further investigation and validation
- GPU parallel computation

Some videos ...

Papers & videos

- A. Bernard-Champmartin, F. De Vuyst, « A low diffusive Lagrange-Remap scheme for the simulation of violent air-water free-surface flows », under progress, to submit to J. Comput. Phys. (2012)
- A. Bernard-Champmartin, F. De Vuyst, A low diffusive Lagrange-remap scheme for the simulation of violent air-water free-surface flows. Applications to dam-break and sloshing events, in preparation.
- Videos :
<http://www.youtube.com/user/floriandevuyst/videos>

Centre de mathématiques et de
leurs applications

CMLA UMR 8536



Cmla

Thank you for your attention